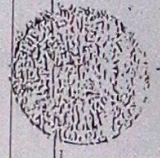




2

Tanta University
Faculty of engineering
Electrical Power and Machines engineering department
Energy Conversion Course



Sheet (3) Electrical Transformers

- 1) The no-load current of a transformer is 10 A at a power factor of 0.25 lagging, when connected to 400 V, 50 Hz supply. Calculate:
P.122
a) Magnetizing component of no-load current. (5m)
b) Iron loss and c) Maximum value of flux in the core assume that primary winding turns are 500.
- 2) A 15 kVA, 2200/110 V transformer has $R_1=1.75 \Omega$, $R_2=0.0045 \Omega$. The leakage reactances are $X_1=2.6 \Omega$ and $X_2=0.0075 \Omega$. Calculate:
P.133
a) Equivalent resistance referred to primary
b) Equivalent resistance referred to secondary
c) Equivalent reactance referred to primary
d) Equivalent reactance referred to secondary
e) Equivalent impedance referred to primary
f) Equivalent impedance referred to secondary
g) Total copper loss
- 3) 250/125 V, 5 kVA single phase transformer has primary resistance of 0.2Ω and reactance of 0.75Ω . The secondary resistance is 0.05Ω and reactance of 0.2Ω .
P.144
a) Determine its regulation while supplying full load on 0.8 leading p.f.
b) The secondary terminal voltage on full load and 0.8 leading p.f.
- 4) A 4 kVA, 200/400 V, 50 Hz, single phase transformer has equivalent resistance referred to primary, as 0.15Ω . Calculate:
P.148
a) The total copper loss on full load
b) The efficiency while supplying full load at 0.9 p.f. lagging
c) The efficiency while supplying half load at 0.8 p.f. lagging
Assume total iron losses = (60 W)
- 5) A 5 kVA, 500/250 V, 50 Hz, single phase transformer gave the following readings,
P.154
O.C. Test: 500 V, 1 A, 50 W (L.V. side open)
S.C. Test: 25 V, 10 A, 60 W (L.V. side shorted)
Determine:
a) η % on full load, 0.8 lagging p.f.
b) The voltage regulation on full load, 0.8 leading p.f.
c) η % on 60% of full load, 0.8 leading p.f.
d) Draw the equivalent circuit referred to primary and insert all the values in it.

$V_1 - V_2$
50

P.161

6) The O.C. and S.C. tests on a 10 kVA, 125/250 V, 50 Hz, single phase transformer gave the following results:

O.C. Test: 125 V, 0.6 A, 50 W (on L.V. side)

S.C. Test: 15 V, 30 A, 100 W (on H.V. side)

Calculate:

- Copper loss on full load
- Full load η % at 0.8 leading p.f.
- Half load η % at 0.8 leading p.f.
- Regulation at full load, 0.9 leading p.f.

P.171

7) A 2500/250 V, 50 Hz, 50 kVA, single phase transformer has a resistance of 0.8Ω and 0.002Ω and a reactance of 4Ω and 0.04Ω for H.V. and L.V. windings respectively. Transformer gives 96% maximum efficiency at 75% full load at unity p.f. The magnetizing component of no load current is 1.2 A on 2500 V side. Find out ammeter, voltmeter and wattmeter readings on O.C and S.C. test if supply is given to the 2500 V side in both cases.

problem ①

Sheet (3) solution

$I_0 = 10 \text{ A}$ at $\text{P.f.} = 0.25 \text{ lag}$, $V_1 = 400 \text{ V}$, $f = 50 \text{ Hz}$
Calculate:

- ① I_m ② Iron loss ③ Max. value of flux in the core if $N_1 = 5000$

① $I_m = I_0 \sin \phi_0$

$\text{P.f.} = \cos \phi_0$

$\phi_0 = \cos^{-1}(0.25) = 75.522^\circ$

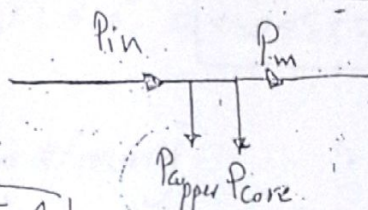
$\therefore I_m = 10 \times \sin(75.522) = 9.6824 \text{ A}$ # ①

- ② at no-load

$P_{\text{iron}} = V_1 \times I_c$

$I_c = I_0 \cos \phi_0 = 2.5 \text{ A}$

$P_{\text{iron}} = 1000 \text{ Watt}$



- ③ $\phi_m = ?$

$E_1 = 4.44 f \phi_m N_1$

$400 = 4.44 \times 50 \times \phi_m \times 5000$

$\therefore \phi_m = 3.6036 \text{ mwb}$

for problem ②

$P_{\text{paper}} = I_1^2 \times R_1 = \left(\frac{15 \times 10^3}{110} \right)^2 \times 0.008875 = 165.031 \text{ watt}$

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or

$P_{\text{paper total}} = I_1^2 \times R_1 + I_2^2 \times R_2$

$= \left(\frac{15000}{2200} \right)^2 \times 1.75 + \left(\frac{15000}{110} \right)^2 \times 0.0045 = 165.031 \text{ W}$

2200/110V, has $R_1 = 1.75 \Omega$, $R_2 = 0.0045 \Omega$, $X_1 = 2.6 \Omega$, $X_2 = 0.0075 \Omega$

a) R_t Referred to primary

$R_1 = 1.75 \Omega$, $R_2' = 0.0045 \times \left(\frac{2200}{110}\right)^2 = 1.8 \Omega$

$\therefore R_{t|_{pri}} = R_1 + R_2' = \boxed{3.55 \Omega}$

b) R_t Referred to secondary

$R_2 = 0.0045 \Omega$, $R_1' = 1.75 \times \left(\frac{110}{2200}\right)^2 = 4.375 \times 10^{-3} \Omega$

$\therefore R_{t|_{sec}} = 8.875 \times 10^{-3} = \boxed{0.008875 \Omega}$

c) X_t Referred to primary

$X_1 = 2.6 \Omega$, $X_2' = 0.0075 \times \left(\frac{2200}{110}\right)^2 = 3 \Omega$

$\therefore X_{t|_{prim}} = \boxed{5.6 \Omega}$

d) X_t Referred to secondary

$X_2 = 0.0075 \Omega$, $X_1' = 2.6 \times \left(\frac{110}{2200}\right)^2 = 6.5 \times 10^{-3} \Omega$

$\therefore X_{t|_{sec}} = \boxed{0.014 \Omega}$

e) Z_t Ref. to primary

$Z_{t|_{prim}} = \sqrt{(R_{t|_{prim}})^2 + (X_{t|_{prim}})^2} = \boxed{6.6304 \Omega}$

f) Z_t Ref. to secondary

$Z_{t|_{sec}} = \sqrt{(R_{t|_{sec}})^2 + (X_{t|_{sec}})^2} = \boxed{0.01657 \Omega}$

e) total copper loss

$P_{copper} = I_{1_{prim}}^2 \times R_{t|_{prim}} = \left(\frac{15 \times 10^3}{2200}\right)^2 \times 3.55 = \boxed{165.031 \text{ watt}}$

check No. prime

250/125 V XFMR, $S = 5 \text{ kVA}$, $1-\phi$, $R_1 = 0.2 \Omega$, $X_1 = 0.75 \Omega$
 $R_2 = 0.05 \Omega$, $X_2 = 0.2 \Omega$

① Regulation for full load on 0.8 P.f. lead

② V_2 on full load and 0.8 P.f. lead

$R_1 = 0.2 \Omega$, $X_1 = 0.75 \Omega$, $R_2 = 0.05 \Omega$, $X_2 = 0.2 \Omega$, $\cos \phi = 0.8$ leading

① \rightarrow Referred to secondary.

$$R'_1 = R_1 \times \left(\frac{125}{250} \right)^2 = 0.05 \Omega$$

$$R_{tsec} = 0.05 + 0.05 = 0.1 \Omega$$

$$X'_1 = X_1 \times \left(\frac{125}{250} \right)^2 = 0.1875 \Omega$$

$$X_{tsec} = 0.3875 \Omega$$

$$I_{sec} = \frac{S}{V_{sec}} = \frac{5 \times 10^3}{125} = 40 \text{ A} = I_2$$

$$\%R = \frac{I_2 R_{tsec} \cos \phi \pm I_2 X_{tsec} \sin \phi}{V_2} \times 100$$

Lag P.f. \rightarrow $+$ \rightarrow Lead P.f.

$$\phi = \cos^{-1}(0.8) = 36.869^\circ$$

$$\sin \phi = 0.6$$

$$\%R = \frac{40 \times 0.1 \times 0.8 - 40 \times 0.3875 \times 0.6}{125} \times 100 = -4.88\%$$

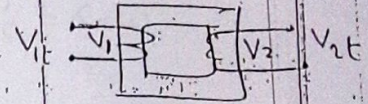
② The same load

$$\%R = \frac{V_2 - V_{2t}}{V_2} \Rightarrow -4.88 = \frac{125 - V_{2t}}{125}$$

Terminal Voltage

$$V_{2t} = 131.1 \text{ V}$$

Leading $\therefore V_{2t} < V_2$ i.e. 131.1 V
 (2 lines)



Lead

-4.88%

200/400 V, 50 Hz XFMR, 1- ϕ
 $R_{tprim} = 0.15 \Omega$, Iron loss = 60 W

- ① P_{copper} total on full load
- ② η full-load at 0.9 P.f lag
- ③ η half load at 0.8 P.f lead

$$\frac{P_{out}}{P_{in}} = \frac{P_{out}}{P_{out} + P_{iron} + P_{copper}}$$

$V_1 = 200 \text{ V}, V_2 = 400 \text{ V}, R_{tpr} = 0.15, P_i = 60 \text{ W}$

$$R_{tsec} = 0.15 \times \left(\frac{400}{200}\right)^2 = 0.6 \Omega \text{ Referred to secondary}$$

$$I_{2fL} = \frac{S}{V_2} = \frac{4000}{400} = 10 \text{ A}$$

$$P_{copper} = I_{2fL}^2 \times R_{tsec} = 10^2 \times 0.6 = 60 \text{ W}$$

$$P_{copper} = I_{fL}^2 R_{tprim} = \left(\frac{2000}{200}\right)^2 \times 0.15 = 60$$

$$\eta = \frac{P_{out}}{P_{in}} = \frac{S \cos \phi}{S \cos \phi + P_i + P_{copper(fL)}}$$

η at $\cos \phi = 0.9$ lag (full-load)

$$\eta = \frac{4 \times 10^3 \times 0.9}{4 \times 10^3 \times 0.9 + 60 + 60} \times 100 = 96.77\%$$

③ when the load reduced to half

$n = \frac{\text{actual load}}{\text{full load}}$ = fraction by which load is less than full-load

$$I_{2new} = n I_{2fL}, \text{ also } P_{copper new} = n^2 P_{copper(fL)}, P_{out new} = n P_{out(fL)}$$

$$\eta = \frac{n \times S \times \cos \phi}{n \times S \times \cos \phi + P_i + n^2 P_{copper(fL)}} = \frac{0.5 \times 4 \times 10^3 \times 0.8}{0.5 \times 4 \times 10^3 \times 0.8 + 60 + (0.5^2) \times 60}$$

$$\eta = 98.52\%$$

2% loss (1%)

$$P_{out} = P_{in} - P_{iron} - P_{copper}$$